

**Amendments to the Specification:**

Please replace the paragraph beginning on page 4, line 2, with the following amended paragraph:

The conductive material with the higher acoustic impedance comprises for example platinum (Pt), ~~wolfram-tungsten~~ (W), molybdenum (Mo), ~~titan-wolfram-titan-tungsten~~ ( $Ti_xW_{1-x}$ ,  $0 < x < 1$ ) or gold (Au).

Please replace the paragraph beginning on page 6, line 21, with the following amended paragraph:

FIG. 4 illustrates a table with the coupling factor  $k_r$  versus the thickness  $T_3$  of the top electrode 15 and versus the thickness  $T_4$  of the bottom electrode 13 of the filter's non-mass-loaded SBARs 8 as shown in FIG. 2. The electrode metal is molybdenum (Mo) which has about twice the acoustic impedance of aluminium nitride, and very high quality aluminium nitride layers can be grown on it. Tantalum pentoxide ( $Ta_2O_5$ ) ( $Ta_2O_5$ ) and silicon dioxide ( $SiO_2$ ) ( $SiO_2$ ) are employed as the high and the low impedance layers of the Bragg reflector. According to the table the optimum thicknesses of Molybdenum are seen to be in the region of  $T_3=200$  nm for the top electrode 15 and of  $T_4=300$  nm for the bottom electrode 13. For this combination the corresponding thickness of the aluminium nitride is 1410 nm, and the corresponding maximum value of  $k_r$  is 0.226.

Please replace the paragraph beginning on page 7, line 8, with the following amended paragraph:

The enhancement of the coupling factor  $k_r$  using the described optimum unequal thicknesses  $T_3$  and  $T_4$  should be even higher when ~~wolfram-tungsten~~ (W) is used instead of molybdenum as ~~wolfram-tungsten~~ has a mechanical impedance some 70% higher than that of molybdenum.